

Boundary Plasma Issues in Burning Plasma Science

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**Issues present in any magnetic fusion
configuration:**

- 1. wide dispersal of power**
- 2. high divertor gas pressures**
- 3. eliminate impurity production**
- 4. screening of impurities**
- 5. burning plasma experiment?**

(1) Wide Dispersal of Power

- parallel power density (q_u) flowing in the SOL in next-step devices is a serious issue
- material surfaces can handle (5 MW m⁻²) steady-state with active cooling, perhaps 20 MW m⁻² pulsed
- divertor plate and magnetic geometry buys factor ~ 100 , i.e. $q_u \sim 0.5$ GW m⁻² steady-state, $q_u \sim 2.0$ GW m⁻² pulsed
- c.f. ITER, $q_u \sim 1$ to 2 GW m⁻², C-Mod ~ 0.5 GW m⁻², DIII-D ~ 0.2 GW m⁻²
- in steady-state ($>$ secs), reduce q_u by ~ 4 by divertor radiation processes (detached or partially detached), i.e. impurities needed (at least in the divertor \rightarrow screening)
- pulsed (\sim secs), can handle power, particularly if strike points are swept (BPX), but T_t will be high \rightarrow impurity production, high Z_{eff} (not desirable mode of operation)
- we know a lot more now than during the BPX design!

(1) Wide Dispersal of Power/(cont)

- high recycling or detached regimes essential:
 - elevated divertor radiation
 - results in high divertor plasma/neutral densities
- criterion for high recycling and cold divertor, $T_t \sim 5$ eV (a prerequisite for detachment):

$$\frac{L^{4/7} n_u^2}{q_u^{10/7}} > 3 \times 10^{29} \quad (\text{SI units})$$

- this is essentially a collisionality parameter:

collisional \rightarrow develop parallel gradients

(1) Wide Dispersal of Power/(cont)

- most important parameter: power width λ_P

$$q_u \sim \frac{P_{\text{SOL}}}{\lambda_P}$$

- λ_P determined by relative rates of cross-field (χ_{\perp}) and parallel heat transport (Spitzer conductivity):

$$\lambda_P \sim \frac{(n_u \chi_{\perp})^{7/9}}{P_{\text{SOL}}^{5/9}}$$

- q_u at high power and especially in H-mode rises strongly: i.e. as $P_{\text{SOL}} \uparrow$ and $\chi_{\perp} \downarrow$, then $\lambda_P \uparrow\uparrow$
- we have very little solid scaling for χ_{\perp} amongst different machines \Rightarrow a real need from present experiments!

(1) Wide Dispersal of Power/(cont)

ELMs

- ELMs exhaust power in short periods of time (< 1 ms)
- Type I: $\Delta E/E = 0.02$ to 0.06 , gives 2 to 6 MJ m⁻² (ITER) on divertor plate, significant erosion expected above 1.5 MJ m⁻²
- mitigating factors:
 - radiation (non-coronal)
 - λ_P broadening
- probably depends on details, particularly density, impurity content, etc \Rightarrow research on present experiments needed

(2) High Divertor Gas Pressures

- while maintaining low main chamber pressure for H-modes (tight baffling??)
- allows efficient pumping to:
 - remove helium ash
 - induce SOL flow towards divertor
 - control density
- helium exhaust time, i.e. τ_{He} , limited by extraction rate at the edge (maybe not with ITB)
- present results are encouraging: $\tau_{\text{He}} < 10 \tau_{\text{E}}$
- scaling to reactor is favorable, i.e. $\tau_{\text{He}} \sim a$, $\tau_{\text{E}} \sim a^2$

(3) Eliminate Impurity Production

- high recycling or detached regime ($T_t < 5$ eV) will ensure target plate physical sputtering is small
- chemical sputtering of carbon a serious issue (no energy threshold), existing graphite machines rarely have $Z_{\text{eff}} < 1.5 \Rightarrow$ avoid graphite (also essential to avoid tritium inventory problems through co-deposition)
- throat region is interface between energetic plasma and neutrals \Rightarrow potential for CX sputtering (perhaps use high Z material here, has high energy threshold)
- interaction at walls of tenuous plasma:
 1. how does plasma reach wall? (rapid \perp transport?)
 2. can dominate core impurity contamination
 3. volatile impurity gases reduced with boronization

(4) Screening of Impurities

- **we need impurities to radiate power:**
 1. **mantle (~ 10% to 50% in present machines) – not desirable since this means (a) core contamination (b) reduction of P_{SOL} (c) confinement degradation**
 2. **divertor – highly desirable**
- **how to have divertor enrichment ($\eta \equiv c_{\text{gas}}/c_{\text{plasma}}$) for impurities (including helium)?**
- **flow entrainment to fight thermal force:**
 1. **natural: rely on the relative mfp's of the impurity atoms compared with the hydrogenic atoms,**
 - (a) **helium dilution, $0.1 < \eta_{\text{He}} < 0.8$**
 - (b) **N, Ne, Ar strong enrichment, $\eta_z = 5$ to 20**
 2. **generate flow: into the divertor,**
 - (a) **strong divertor pumping with main chamber fuel puffing**
 - (b) **neutral gas manipulation, e.g. plate/baffle geometry, by-passes**
- **validate present codes for application to the Next-Step**

(5) Why do we need a Burning Plasma Experiment?

because....

λ_P , ELMs, main chamber recycling \Rightarrow we really cannot predict these with any certainty